

TD 603  
Water Resources

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Lecture 6: Mathematics of Groundwater flow

# The basic variables and continuity

- $h(x, y, z, t)$ : The head at a point in time.
- $q(x, y, z, t)$ : The inflow/outflow at a point in time.
- $z$ : the elevation of the point  $(x, y, z)$ .
- velocity  $v_x(x, y, z, t)$ : in the  $x$ -direction.

$$v_x = K_x \partial h / \partial x$$

- saturated/water-table/unsaturated region: where  $h \geq z, h = z, h < z$ .

- Boundary  $\partial B$  of the terrain  $B$ .
- Boundary conditions: known  $h$  or known  $q$ .

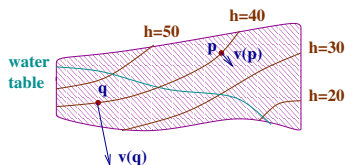
## Continuity Equation

What is

$$\frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z}?$$

It is the rate of accumulation of water at the point  $(x, y, z, t)$ !

# The condition



Thus assuming an ideal moisture condition, i.e.,

- **unsaturated:**  
moisture = 0.
- **saturated:**  
moisture = porosity.

we must have that water accumulation is zero if  $q = 0$ .

Thus we have at **both**  $p$  and  $q$ :

$$\frac{\partial}{\partial x} \left( K_x \frac{\partial h}{\partial x} \right) + \frac{\partial}{\partial y} \left( K_y \frac{\partial h}{\partial y} \right) + \frac{\partial}{\partial z} \left( K_z \frac{\partial h}{\partial z} \right) = 0$$

Let us assume that  $K_x, K_y, K_z$  are constants. Whence, we have *for all points NOT on the water table*:

$$K_x \frac{\partial^2 h}{\partial x^2} + K_y \frac{\partial^2 h}{\partial y^2} + K_z \frac{\partial^2 h}{\partial z^2} = -q$$

E.g.,  $\partial^2 h / \partial x^2 > 0$  implies

$$v_x(x + dx) - v_x(x) < 0$$

Thus requiring an external outflux of water, i.e.,  $q > 0$ .

# At the water table

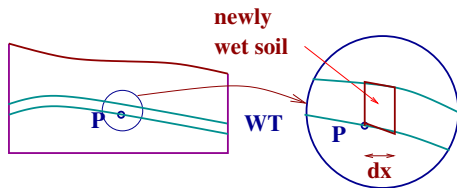
Points  $P$  on the water table may lose or gain water if  $h$  changes.

- If  $h$  increases then the water table has risen.
- More water is required for this raise.
- and the converse

For points on the water table, the outflux, i.e.,:

$$K_x \frac{\partial^2 h}{\partial x^2} + K_y \frac{\partial^2 h}{\partial y^2} + K_z \frac{\partial^2 h}{\partial z^2}$$

must be accounted by the rise or fall of the water-table.

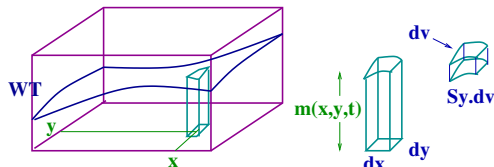


There is much argument about how this is to be modelled.

- We take the co-called **Regional Groundwater Equation**.
- Key Assumption: The flows in the  $z$  directions are small, i.e.,  $h$  is roughly constant along  $z$ .

# One Try

- $m(x, y, t)$ : ht. of water table at time  $t$ .
- $S_y \frac{\partial m}{\partial t}$ : Amount of water needed at  $x, y, z, t$  to move the water table.
- But is  $m(x, y, t)$  computable?: Yes
- $m(x, y, t)$  is merely the  $z_0$  so that  $h(x, y, z_0, t) - z_0 = 0$
- **So not a new variable!**



Note that

$$A(t) = \int_x \int_y S_y \frac{\partial m}{\partial t} dx dy$$

is the amount of water which has come in (or gone out) from the column in the time interval  $[t, t + dt]$ .

Also note that:

$$B(t) = \int_{\partial T} q(x, y, z, t) ds$$

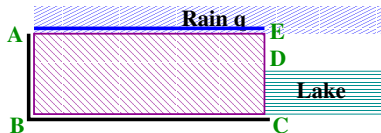
the integral on the boundary  $\partial T$  of the terrain of the net water influx.

$$A(t) = B(t)!$$

$$m \cdot K_x \frac{\partial^2 h}{\partial x^2} + m \cdot K_y \frac{\partial^2 h}{\partial y^2} = S_y \frac{\partial m}{\partial t} - q$$

- This equation is a *synthesis* of the governing equations for all regions.
- We will call this the **The Idealized Unconfined Regional Groundwater flow equation**.
- It is of limited computational value. These will focus on the saturated region.

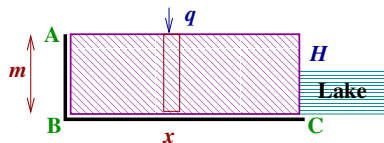
Even then, many models make simplifying assumptions.



### Boundary Conditions

- AB, BC is no flow.
- AE is with water influx  $q$  mm/day.
- CD is with a known constant head  $h = H$ , the height of the water in the lake.

# The Model



## Assumptions

- Assume that the thickness  $m$  of the saturated layer is large compared to the variation in its height.
- Consider the **saturated** column situated at  $x$ . **Then:**

$$\frac{d}{dx} \left( mK_x \frac{dh}{dx} \right) = mK_x \frac{d^2 h}{dx^2} = -q$$

Two inherent points:

- $m \sim h$ , so  $m$  assumed to be the thickness.
- the head  $h$  is assumed constant in this column.

Whence:

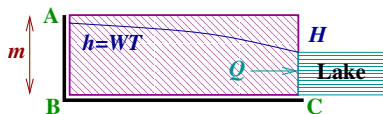
$$h(x) = \frac{-q}{2mK_x} x^2 + Ax + B$$

For some constants  $A, B$  to be determined. We have (i)  $h(L) = H$  and (ii) flow at  $AB$  is zero. In other words:

$$\frac{dh}{dx}(0) = \left( \frac{-q}{mK_x} x + A \right) (0) = 0$$

This implies  $A = 0$ .

# Several Points



Solving for (i) gives us:

$$h = H + \frac{q(L^2 - x^2)}{2mK_x}$$

- Note that this  $h$  is actually the head  $h(x, y)$ .
- Thus  $y - h(x, y) = 0$  gives us the WT.
- The inflow into the lake is

$$Q = mK_x \cdot \frac{dh}{dx}(L) = -qL$$

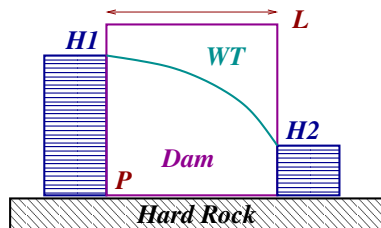
- Actual lake is a 3D problem, to be solved numerically.
- The assumptions imply large soil thickness and hard-rock stratum common to both lake and bank.

## Problem

- What do realistic values of  $L$ ,  $m$  and  $K$  give as the variation for  $h$ . Are the assumptions reasonable?
- Do the problem for  $q = ax + b$ , when say, the rains reduce as we move from  $x = 0$  (the mountains?) to  $x = L$  (the lake).



# The Dupuit scheme



- A dam of width  $L$  has water stored at height  $H_1$  on the upstream side.
- The downstream has head  $H_2$ .
- The whole dam is on impermeable rock.
- Compute the head  $h(x, y)$  at all points in the dam.

The point  $P$  is  $(0, 0)$ .

## The 1-Dupuit Assumptions

- The parameter here is  $x$ .
- The head  $h(x, y)$  depends only on  $x$ . Thus the water-table at point  $x$  is at height  $h(x)$ .

Again, by taking a column at  $x$ , we have:

$$\frac{\partial}{\partial x}(hK_x \frac{\partial h}{\partial x}) = -q(x)$$

This implies

$$\frac{\partial^2 h^2}{\partial x^2} = \frac{-2q}{K_x}$$

# The 1-D Dupuit

The basic equation:

$$\frac{\partial^2 h^2}{\partial x^2} = \frac{-2q}{K_x}$$

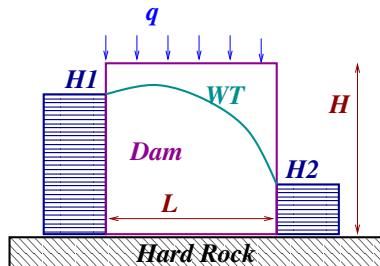
The dam problem has  $q(x) = 0$ .  
Thus

$$h^2(x, y) = \frac{-2q}{K_x} x^2 + Ax + B$$

$h(0) = H_1$  and  $h(L) = H_2$  imply:

$$h^2(x) = H_1^2 - \frac{H_1^2 - H_2^2}{L} x$$

Thus, if  $L = 1$  and  $H_2 = 0$  and  $H_1 = 1$  then  $h(x) = \sqrt{1 - x}$ .  
This explains the shape of the curve.



## Problem

Now assume that the dam receives a rainfall of  $q$ . The height of the dam is  $H$ .

- Compute the water-table.
- For what rains would the top of the dam seep water?

# Transmissivity

Note that the terms

- $mK_x$  in the lake problem.
- $hK_x$  in the dam problem.

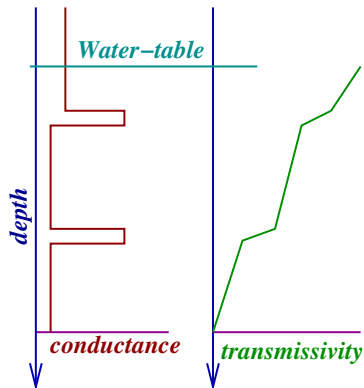
is **transmissivity ( $T$ ) of the aquifer** .

In other words, it measures the power of the aquifer to respond to a differential in the head.

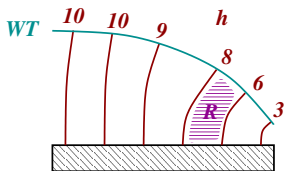
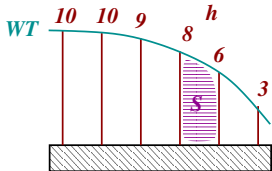
- It depends on the location of the water-table.
- In principle, the transmissivity depends on the thickness of the saturated part of the aquifer, and changes with time.

The general definition is

$$T = \int K(l)dl$$



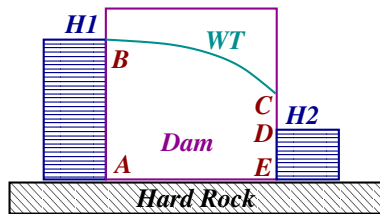
# But is Dupuit correct?



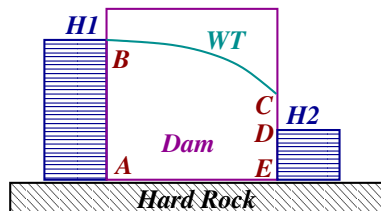
- The assumptions of  $h$  being constant vertically is wrong and is true only when the slope of  $WT$  is small.
- We will see soon that iso- $h$  lines intersect the  $WT$  at 90 degrees.
- The *Dupuit* approximation actually approximates region  $R$  by regions  $S$ .

The actual water-table for the simple dam is shown below.

*Water seeps out of the face CD!*



# The Dam Again



AB : constant head  $H_1$ .

AE : no flow ( $\partial h / \partial z = 0$ ).

DE : constant head  $H_2$ .

CD : seepage face, var. head  $z$ .

Water seeps out at  $CD \Rightarrow$  head there equals atmospheric pressure, i.e.,  $z$ .

The problem is that point  $C$  and curve  $BC$  are **unknown**. Whence, the curve  $BC$  will need two defining conditions.

- $h = z$ :  $BC$  is the water-table.
- $\partial h / \partial n = 0$ : No flow across  $BC$ .

where  $n$  is the normal to the water-table.

In other words, velocity vectors at points on the  $WT$  are along it.

The second condition  $\Rightarrow$

$$\nabla h \cdot \nabla (h - z) = 0$$

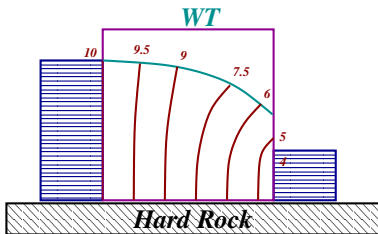
(where  $\nabla$  is the *gradient*)

# Finally

This simplifies to:

$$\left(\frac{\partial h}{\partial x}\right)^2 + \left(\frac{\partial h}{\partial z}\right)^2 = \frac{\partial h}{\partial z}$$

- The conditions  $h - z = 0$  and  $\frac{\partial h}{\partial n} = 0$  are standard for locating the missing water-table in general situations.
- They say that the water-table hits all equi-potential surfaces at right angles.



- There is no analytic solution and only a **computational one**. The heads are shown in the figure above.
- Note that the equi-p lines meet the WT and leave the rock-bottom at 90-degrees.
- Also see that the  $h = 5$  lines meets the seepage face at an angle. This gives the seepage at the point.

# Discussion

- 1 Are there situations when  $K_x$  varies with  $x$ ?
- 2 Are there any other properties of water/soil which seem to be ignored?
- 3 In the lake problem, how is it that we assume  $m$  as fixed and then  $h$  as varying.
- 4 What do you think is the general seepage condition?
- 5 Look at the “exact” dam solution. What would you do if the model had to include constant rain  $q$ ?
- 6 Is there any additional condition for locating point  $C$ ?